Modeling of contact interaction of two bodies with possibility of sliding

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Theoretical part

- Classical statement of contact problems
- Integrated statement
- Variation statement
- Solvability of contact problems on basis of minimization of convex functional

Practical part

- Description of fast algorithm for solving contact problems
- Investigation of applicability of the algorithm to models with great curvature of surfaces
- Analysis of influence of tangential displacements to the solution
- Comparing the results obtained with developed algorithm and finite element complex ANSYS

Problem 1. Deformation of elastic body without obstacle



Solution:

- Small deformations in the body: $\underline{\varepsilon} = \frac{\nabla \underline{u} + \nabla^T \underline{u}}{2}$
- Hook's law:

$$\underline{\underline{\sigma}} = \underline{\underline{L}} : \underline{\underline{\varepsilon}}$$

- Balance equations: $\operatorname{div}(\sigma(\underline{u})) = -\underline{K}$
- Boundary conditions:

$$\underline{u}\big|_{\partial_1\Omega}=0$$

$$\underline{\sigma_n}\Big|_{\partial_2\Omega} = \underline{F_n}$$

Problem 2. Contact of elastic body and rigid obstacle



- Balance equations: $\operatorname{div}(\underline{\sigma}(\underline{u})) = -\underline{K}$
- Boundary conditions:

$$\underline{u}\Big|_{\partial_1\Omega}=0$$

$$\underline{\sigma_n}\Big|_{\partial_2\Omega} = \underline{F_n}$$

Condition of non-penetration:

$$u_n\Big|_{\partial_3\Omega} \leq g_n$$

Signorini conditions:

$$\begin{bmatrix} \sigma_n \\ \sigma_n = 0, e c \pi n, \sigma_n \leq 0; \end{bmatrix}$$

4

Problem 3. Contact of two rigid bodies



- Balance equations: div(<u>σ(u))</u>= −<u>K</u>
 Boundary conditions:
- Boundary conditions $\underline{u}|_{\partial \Omega} = 0$

$$\underline{\sigma_n}\Big|_{\partial_2\Omega} = \underline{F_n}$$

• Conditions in contact area: $u_n|_{\partial_3\Omega_1} + u_n|_{\partial_3\Omega_2} \leq g_n$ $\begin{cases} \underline{\sigma_n}|_{\partial_3\Omega} = \sigma_n \underline{n}, \quad \sigma_n \leq 0; \\ \sigma_n = 0, \ \text{если} \ u_n|_{\partial_3\Omega_1} + u_n|_{\partial_3\Omega_2} < g_n; \\ \sigma_n|_{\partial_3\Omega_1} = \sigma_n|_{\partial_3\Omega_2} \qquad 5 \end{cases}$



Integrated statements of contact problems

• Problem 1 $\underline{u} \in \left[W_2^1(\Omega)\right]^n$ $\hat{W}_2^1(\Omega) = \left\{w \in W_2^1(\Omega); w\right|_{\partial,\Omega} = 0\right\}$ $\int_{\Omega} \underline{\underline{L}} : \underline{\underline{\varepsilon}}(\underline{u}) :\underline{\underline{\varepsilon}}(\underline{v}) dx = \int_{\Omega} \underline{K} \cdot \underline{v} \, dx + \int_{\partial_{\gamma}\Omega} \underline{F_n} \cdot \underline{v} \, ds, \quad \forall \, \underline{v} \in \left[W_2^1(\Omega)\right]^n \quad \blacksquare \quad a(\underline{u}, \underline{v}) = l(\underline{v})$ • Problem 2 $\underline{u} \in \Re$ $\Re = \left\{ \underline{w} \in \left[W_2^1(\Omega) \right]^n; \underline{w} \Big|_{\partial_1 \Omega} = 0; w_n \Big|_{\partial_2 \Omega} \le g_n \right\}$ $\int_{\Omega} \underline{\underline{L}} : \underline{\underline{\varepsilon}}(\underline{u}) :\underline{\underline{\varepsilon}}(\underline{v} - \underline{u}) dx \ge \int_{\Omega} \underline{K} \cdot (\underline{v} - \underline{u}) dx + \int_{\Omega} \underline{F_n} \cdot (\underline{v} - \underline{u}) ds, \quad \forall \underline{v} \in \Re \implies a(\underline{u}, \underline{v} - \underline{u}) \ge l(\underline{v} - \underline{u})$ • Problem 3 $\underline{u} \in \mathfrak{I}$ $\mathfrak{I} = \left\{ \underline{w} \in \left[W_2^1(\Omega) \right]^n; \ \underline{w} \Big|_{\partial_1 \Omega} = 0; \ w_n^1 \Big|_{\partial_3 \Omega_1} + \left. w_n^2 \right|_{\partial_3 \Omega_2} \le g_n \right\}$ $\int_{\Omega} \underline{\underline{L}} : \underline{\underline{\varepsilon}}(\underline{u}) :\underline{\underline{\varepsilon}}(\underline{v} - \underline{u}) dx \ge \int_{\Omega} \underline{K} \cdot (\underline{v} - \underline{u}) dx + \int_{\partial_{2}\Omega} \underline{F_{n}} \cdot (\underline{v} - \underline{u}) ds, \quad \forall \underline{v} \in \mathfrak{I} \longrightarrow a(\underline{u}, \underline{v} - \underline{u}) \ge l(\underline{v} - \underline{u})$

Minimization of functional Problem 1 Problem 2 Problem 3 $a(\underline{u},\underline{v}) = l(\underline{v}), \forall \underline{v} \in [W_2^1(\Omega)]^n$ $a(\underline{u}, \underline{v} - \underline{u}) \ge l(\underline{v} - \underline{u}), \forall \underline{v} \in \Re$ $a(\underline{u}, \underline{v} - \underline{u}) \ge l(\underline{v} - \underline{u}), \forall \underline{v} \in \mathfrak{I}$ $\min_{v \in A} I(\underline{v}), \quad I(\underline{v}) = \frac{1}{2} a(\underline{v}, \underline{v}) - l(\underline{v})$

- Set A $\left(\left[W_2^1(\Omega) \right]^n, \mathfrak{R}, \mathfrak{I} \right)$
- Self-contained
- Convex

Functional I

- Continuous
- Strict convex
- Bottom bounded
- Coercive

$$\exists ! \underline{u} \in A, \\ I(\underline{u}) = \min_{\underline{v} \in A} I(\underline{v})$$



<u>Output</u>: gap field in the contact area $G = g_n - U$

Problems of applicability to the models with great curvature

Algorithm features

- Modeling of junction of the models with slight curvature of surfaces
- Applying loads in normal direction
- Computing displacements in normal directions

Difficulties in junction of the models with great curvature

Great tangential displacements



Ambiguity in gap definition



Test model description





$$G_{unif} = 7 \, MM$$





Tangential displacements in gap calculation

Value of tangential displacements

$$rel = \frac{u_{\tau}}{u_n} 100\%$$

1

2

3

4

1

2

3

4

3.29

3.62

3.47

3.55

36.94

150.45

63.86

87.07

Difference in solutions with and without including tangential displacements

 $\alpha = 5^0$ F = 3 kg

$$\varepsilon = \frac{\left|G^n - G^{xyz}\right|}{G_{unif}} 100\%$$

$$\alpha = 90^{\circ}$$

F = 17 kg

4	0.15
1	0.13
2	0.27
3	0.10
4	0.26

 $\alpha = 90^{\circ}$ F = 5 kg

 $\alpha = 5^0$ F = 5 kg

Comparing the methods of gap definition

 As the difference between initial gap and normal displacements:

 $G = g_n - U$

According to the model geometry:



Difference in solutions with the two methods

$$\varepsilon = \frac{\left| \frac{G^{dif} - G^{geom}}{G_{unif}} \right| 100\%}{G_{unif}}$$

$$\alpha = 5^{0} \qquad \alpha = 90^{0}$$

$$F = 22 kg \qquad F = 50 kg$$

$$\frac{1}{2} 0.01}{3} \qquad \frac{1}{2} 0.34}{3} 0.00}$$

$$\frac{1}{4} 0.01} \qquad \frac{1}{4} 0.80$$

Comparing results of solution with ANSYS

 Developed algorithm







Difference in solutions with the two algorithms $\varepsilon = \frac{\left|G^{ANSYS} - G\right|}{G_{unif}} 100\%$ $\alpha = 5^{\circ}$ $\alpha = 90^{\circ}$ F = 5 kg F = 29 kg2.33 0.70 2 4.91 2 2.90 3.31 3 3 1.60 1.39 4 4 4.19



- Mathematical statements of contact problems without friction were investigated
- Solvability of these contact problems was proved on basis of minimization of convex functional
- Applicability of developed fast algorithm for solving contact problems to modeling of junction of models with great curvature was investigated
- Good correspondence of the results obtained with developed algorithm and finite element complex ANSYS was demonstrated
- Tangential displacements don't influence on the gap value, what allows to apply the developed algorithm to modeling of junction of models with great curvature



Thank you!